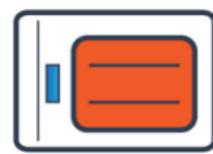


ChE-310

Fundamentals of Separation Processes



Distillation



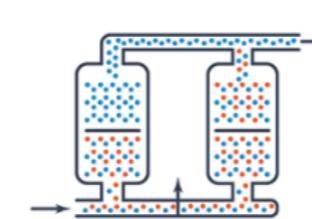
Drying



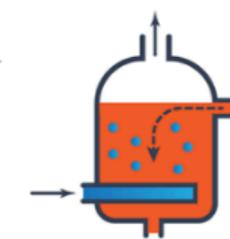
Evaporation



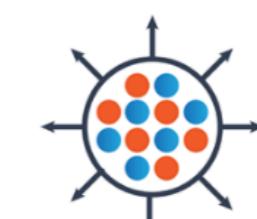
Extraction



Adsorption



Absorption



Membranes

Moodle & course syllabus

All information available on Moodle <https://moodle.epfl.ch/course/view.php?id=15847>

Summary

Students will learn the fundamentals concepts related to molecular separations in industrial processes. Students will employ these concepts to design equilibrium-stage and rate-limited processes for the separation of homogeneous mixture.

Intended Learning Outcome

By the end of the course, students should be able to

- Ø Use of energy separating agent (ESA) and mass separating agent (MSA) for separating chemical mixtures.
- Ø Calculate composition of streams leaving a separation process using the concepts of mass and energy balances, phase equilibria, mass transfer and diffusion.
- Ø Design equilibrium-stage separation process (number of stages, concentration of streams entering or leaving the processes) for the desired outlet concentration from a given feed.

Course Content

Mass and Energy Balances

Thermodynamics of Separations/Phase Equilibria/Degree of Freedom

Flash Distillation

Column Distillation

Multicomponent Distillation

Absorption and Stripping

Liquid-Liquid Extraction

Diffusion and Mass Transfer

Adsorption Processes

Membrane Processes

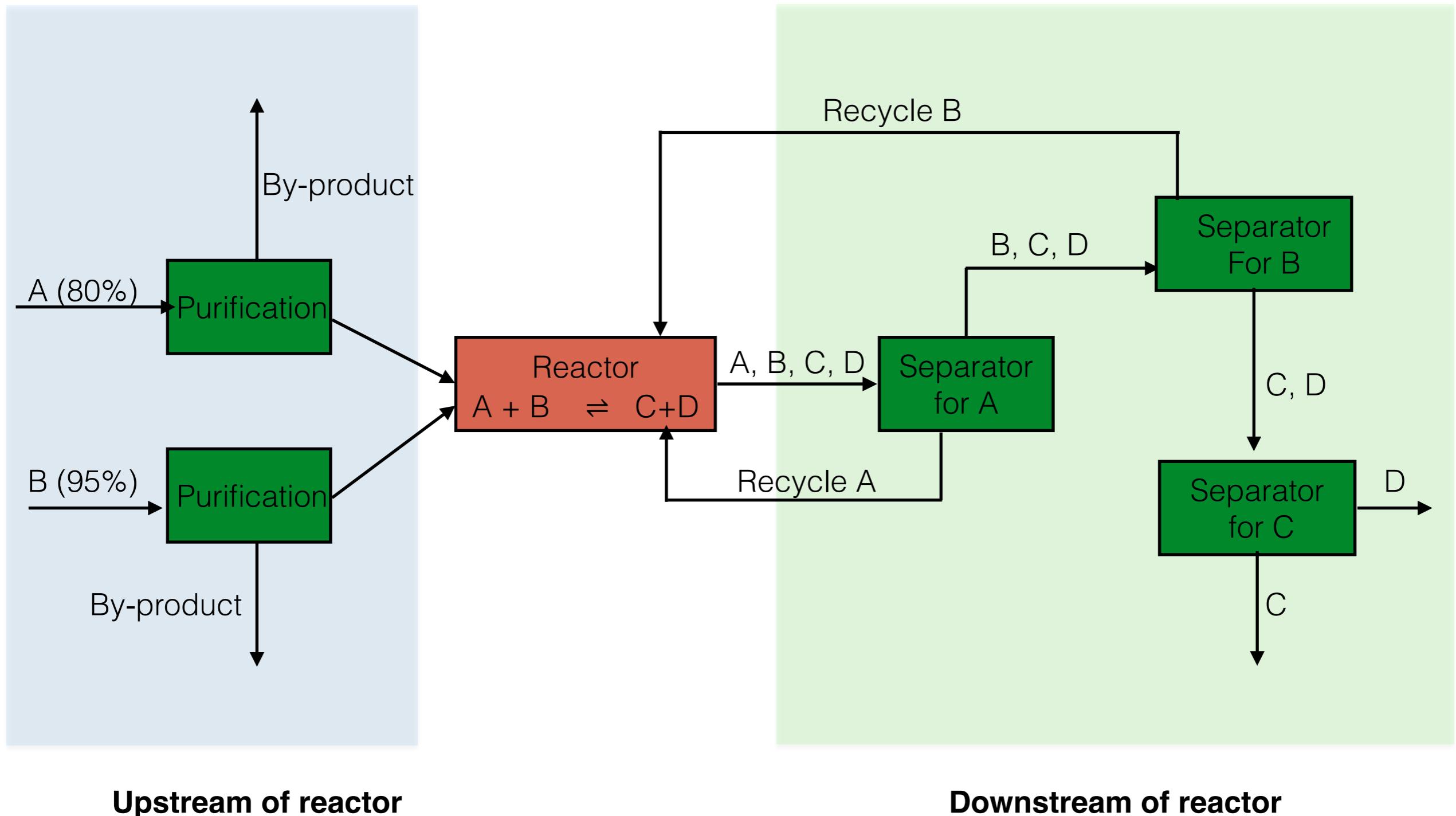
Intended Learning Outcome

1. Introduction to separation processes, and why it is important for chemical engineers.
2. Equilibrium driven separation: The concept of phase equilibria.
3. Composition-temperature, composition-pressure, composition-enthalpy based phase diagrams.

Separation processes consume energy. In a chemical industry where there are typically many processes (for example chemical reactors), what fraction of the total energy use comes from the separation processes.

- A. $\leq 10\%$
- B. 10-25%
- C. 25-40%
- D. $\geq 40\%$

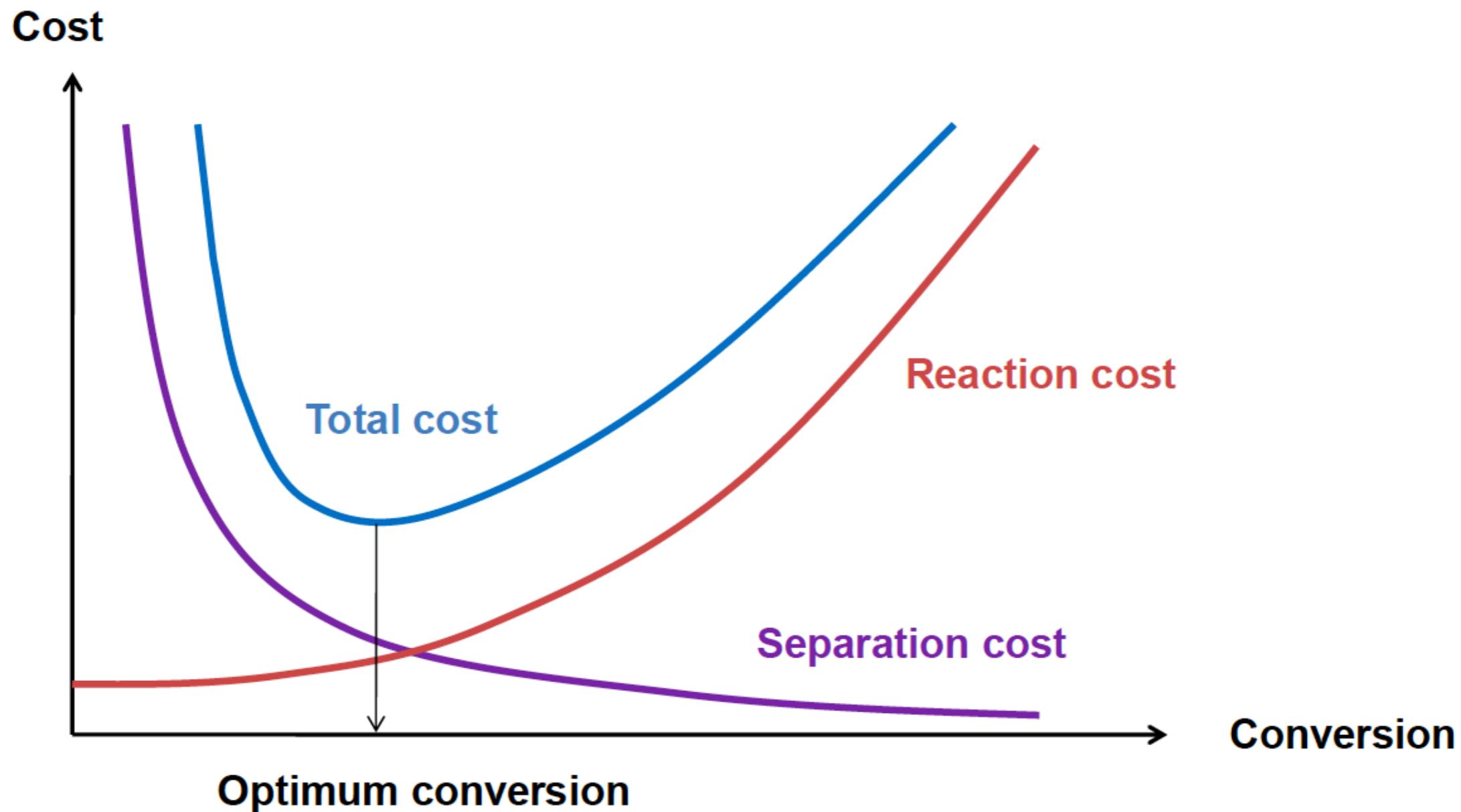
Importance of separation in chemical industry



Upstream of reactor

Downstream of reactor

Overall process economics



DOW Chemicals: Olefin production via steam cracking of naphtha followed by cryogenic distillation

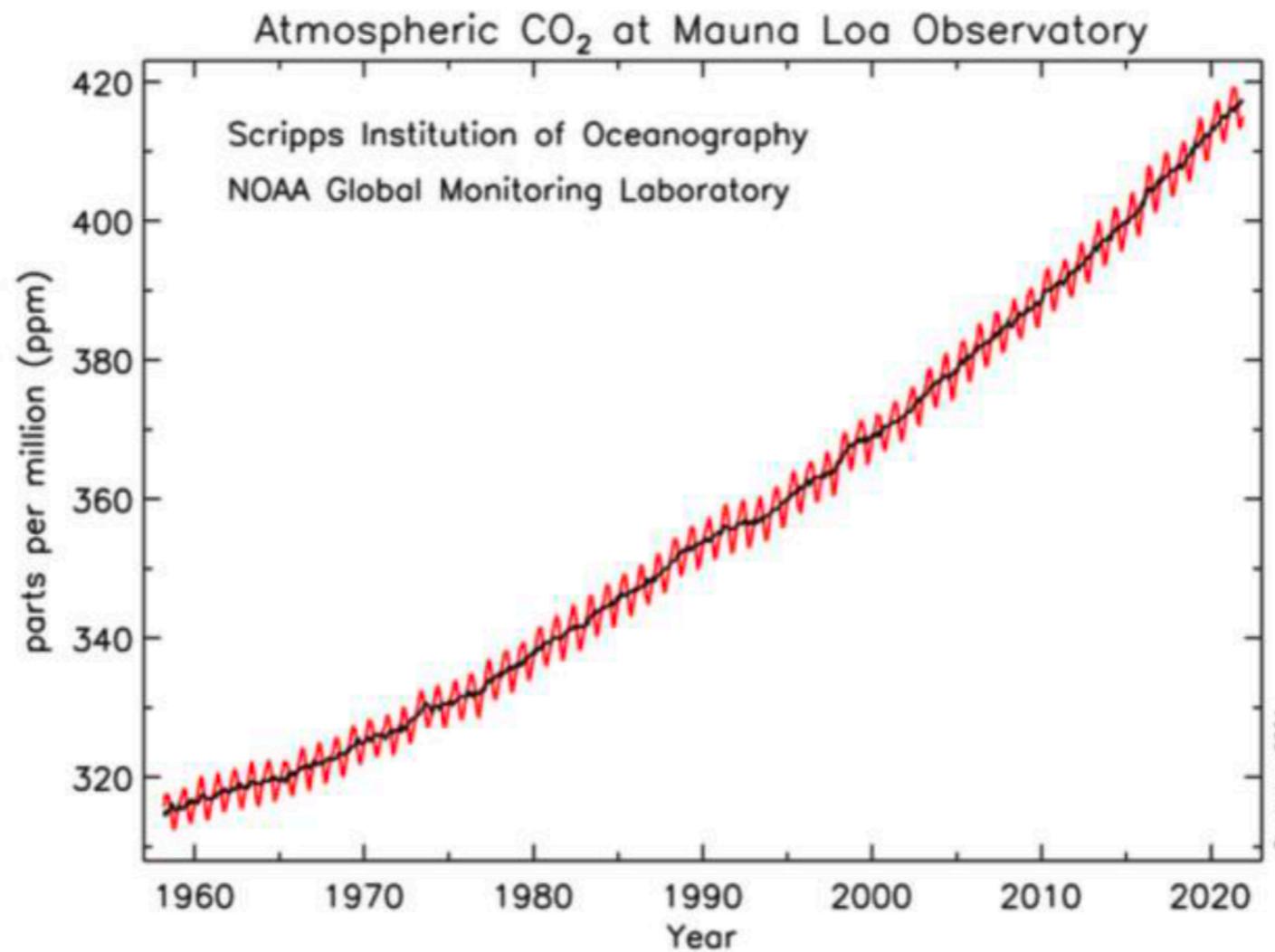


The separation of the C₂ – C₄ paraffin/olefin mixtures by cryogenic distillation is one of today's indispensable and most energy-intensive processes in the refinery industry, consuming up to **85%** of the total energy needed for the entire production process.

Van Miltenburg...

Adsorptive separation of light olefin/paraffin mixtures,
Chem. Engin. Res. & Design 84 (2006) 350

Importance of separation for environment: Carbon capture

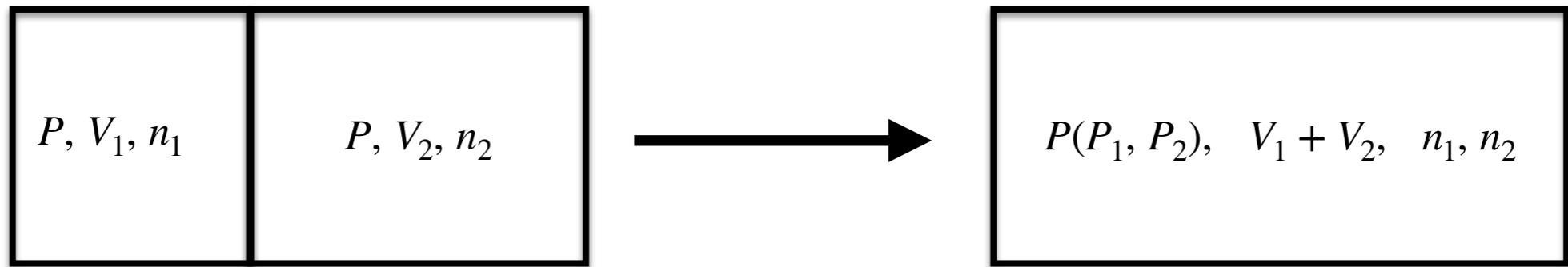


*Figure 2. Monthly mean carbon dioxide measured at Mauna Loa Observatory, Hawaii
(Source: National Oceanic and Atmospheric Administration)*

Mixing vs. Separation

Explain using thermodynamic principles, why mixing to form a homogeneous mixture is a spontaneous process, while separation of that mixture is not.

Consider the case of isothermal mixing



$$G = n \left(\mu^0 + RT \ln \frac{P}{P^0} \right)$$

Change in gibbs free energy = $\Delta G = G_{\text{final}} - G_{\text{initial}}$

$$\Rightarrow \Delta G = \left[n_1 \left(\mu_1^0 + RT \ln \frac{P_1}{P_1^0} \right) + n_2 \left(\mu_2^0 + RT \ln \frac{P_2}{P_2^0} \right) \right] - \left[n_1 \left(\mu_1^0 + RT \ln \frac{P}{P_1^0} \right) + n_2 \left(\mu_2^0 + RT \ln \frac{P}{P_2^0} \right) \right]$$

$$\Rightarrow \Delta G = n_1 RT \ln \left(\frac{P_1}{P} \right) + n_2 RT \ln \left(\frac{P_2}{P} \right) \quad \Rightarrow \Delta G = (n_1 + n_2)(RT) \left(\frac{n_1}{n_1 + n_2} \ln x_1 + \frac{n_2}{n_1 + n_2} \ln x_2 \right)$$

$$\Rightarrow \Delta G = (n_1 + n_2)RT(x_1 \ln x_1 + x_2 \ln x_2)$$

$\Rightarrow \Delta G \leq 0$ **Mixing is spontaneous**

Find the theoretical energy penalty (kJ/kgCO₂) for separating CO₂ (0.04% in air) from air. Direct air capture industries quotes energy penalty which is at least 8 MJ/kgCO₂.

What is their energy efficiency?

$$\Delta G = (n_1 + n_2)RT(x_1 \ln x_1 + x_2 \ln x_2)$$

Basis:	100 mole air
	0.04% CO ₂

mole CO ₂ =	0.04
Mole remaining air =	99.96

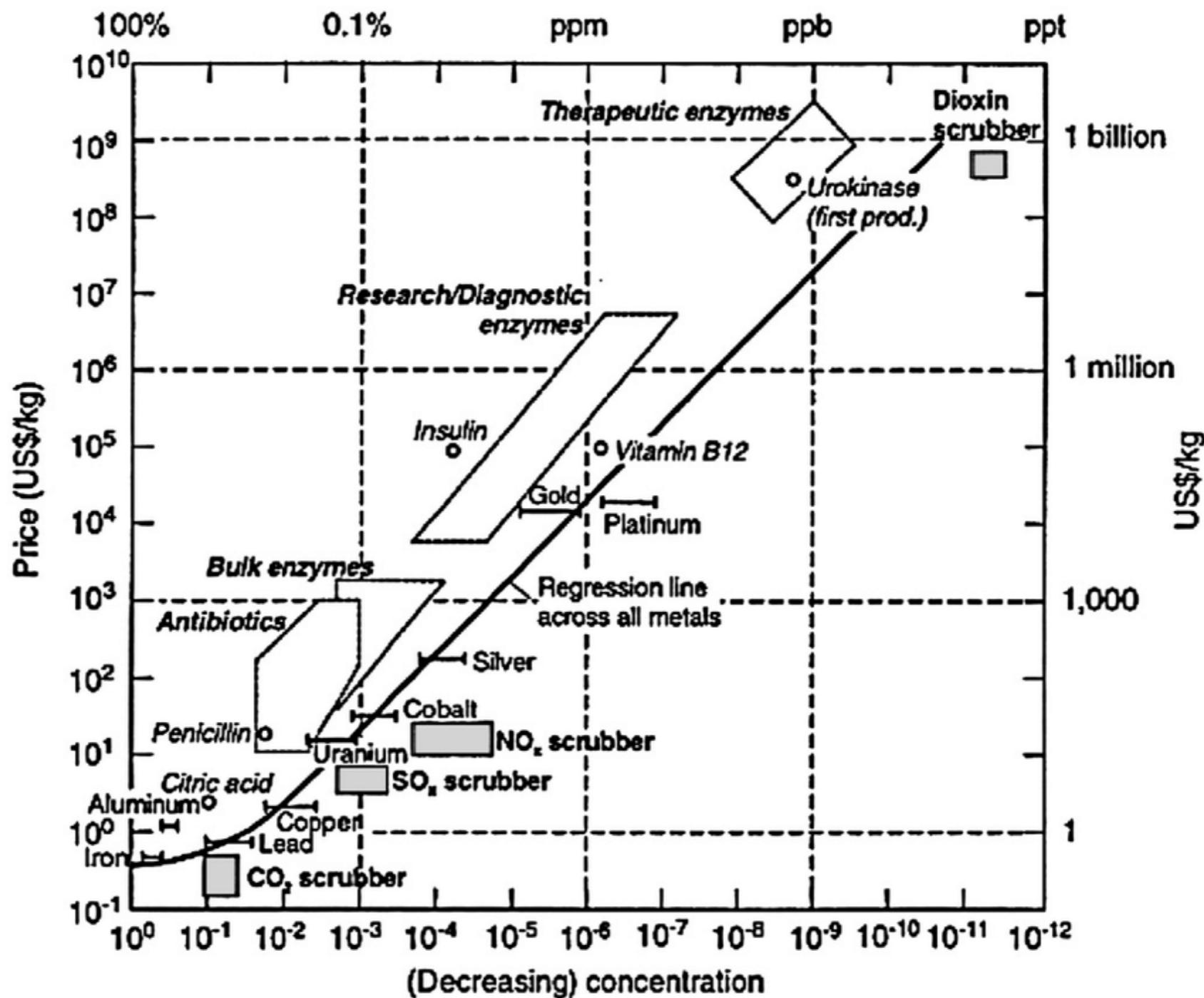
ΔG =	-874.04783 Joules for 0.04 mole of CO ₂
------	--

-21.851196	KJ/mole
-0.4966181	KJ/g
-0.4966181	MJ/kg

Efficiency of commercial process = 0.5/8 = 6.25%

In most cases, the cost/energy needed for separation decides the chemical cost

Sherwood plot

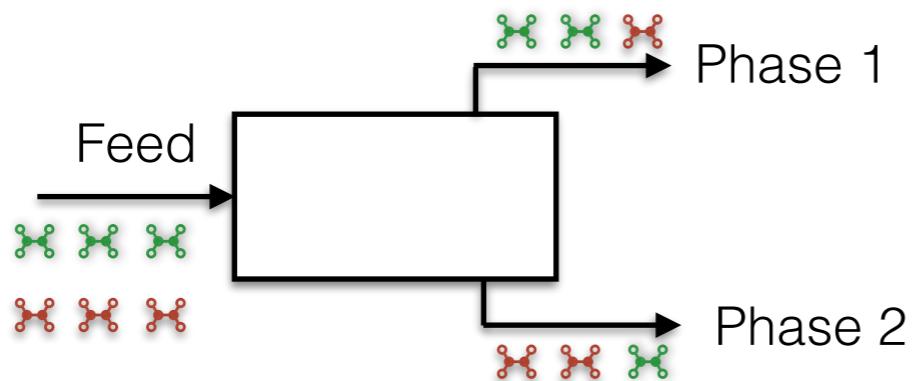


Separation process exploit differences in the chemical and the physical properties

Type	Examples	Properties
Solid-Solid	Powder mixtures	Size, density, binding
Solid-Liquid	Colloidal suspensions	Size, density, binding
Dissolved solid (ions) - Liquid	Seawater	Ionic size, solubility
Liquid-Liquid	Crude oil	Relative volatility, solubility
Gas-Liquid	Dissolved CO ₂	Solubility (pressure, temperature)
Gas-Gas	Air	Boiling point, molecular size, binding

Type of separation process

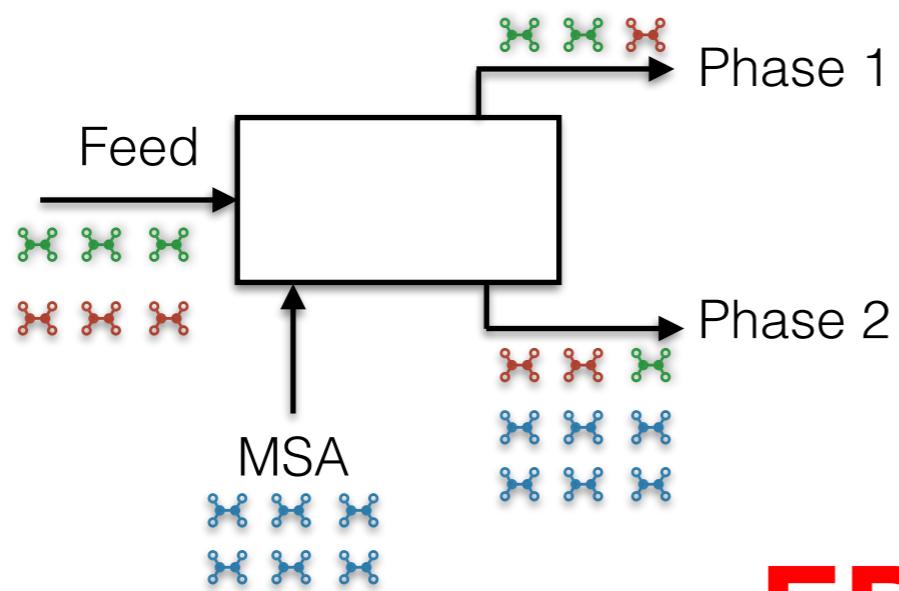
(1) Phase creation by adding/withdrawing energy separating agent (ESA) (change in temperature, pressure)



Examples:

1. Flash vaporization
2. Partial vaporization
3. Partial condensation
4. Distillation
5. Crystallization

(2) Phase creation by adding mass separating agent (MSA)

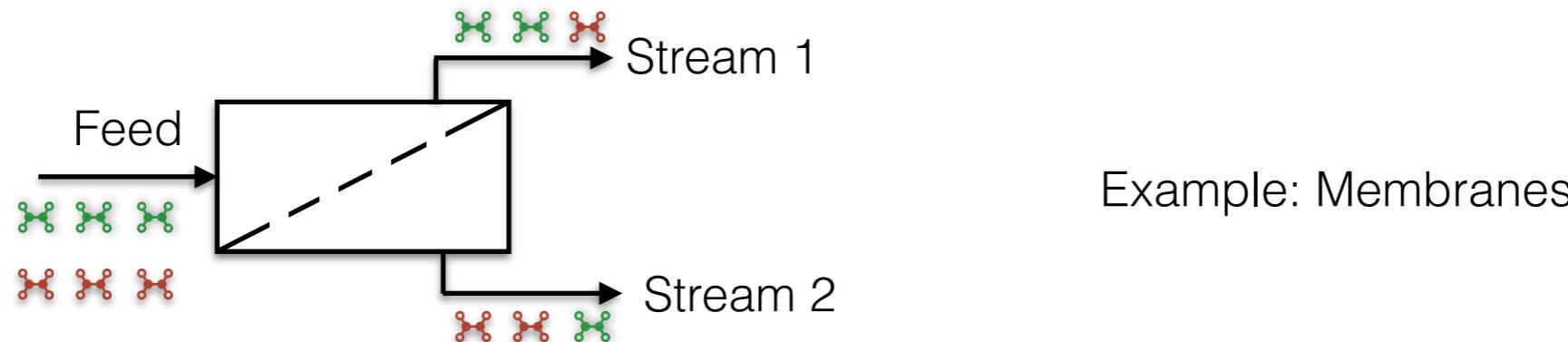


Examples:

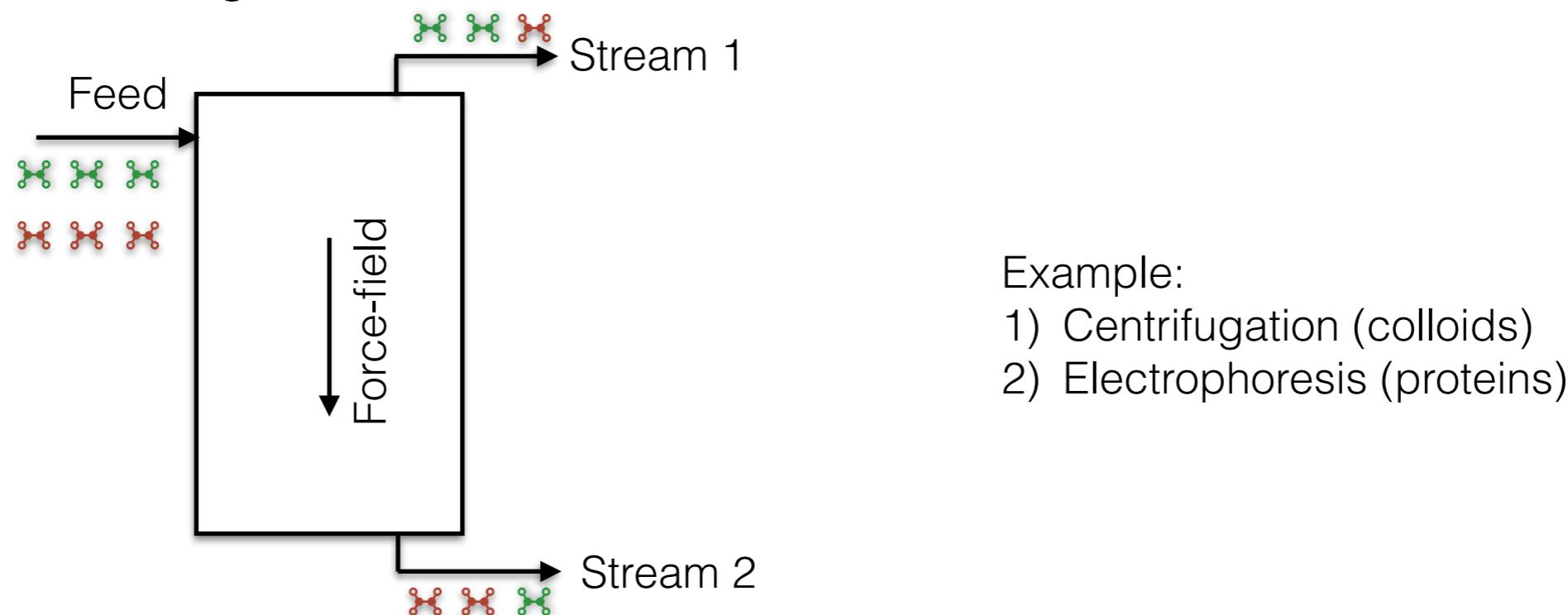
1. Absorption
2. Liquid-Liquid Extraction
3. Adsorption

Type of separation process

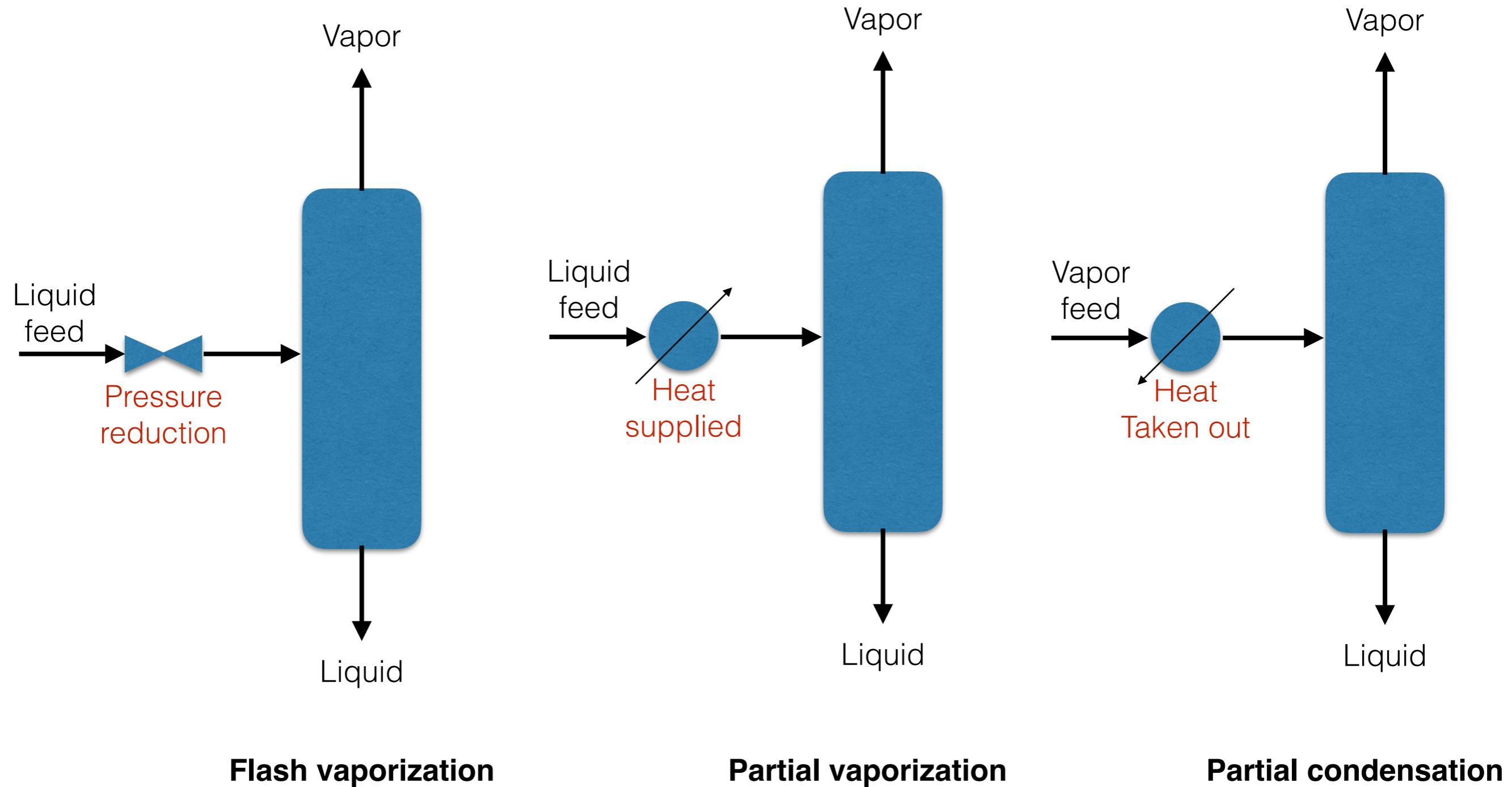
(3) Separation using size difference (selective barrier)



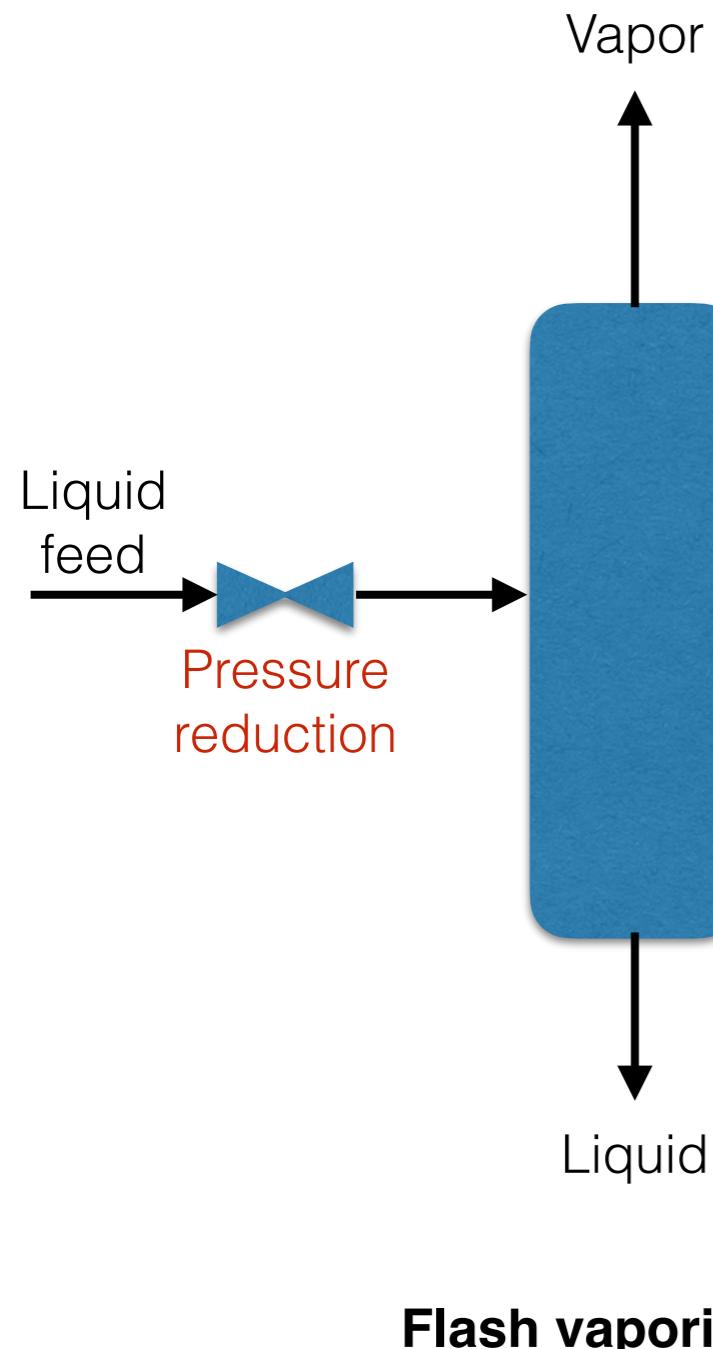
(4) Separation using force-field



Phase creation by energy separating agent (ESA)



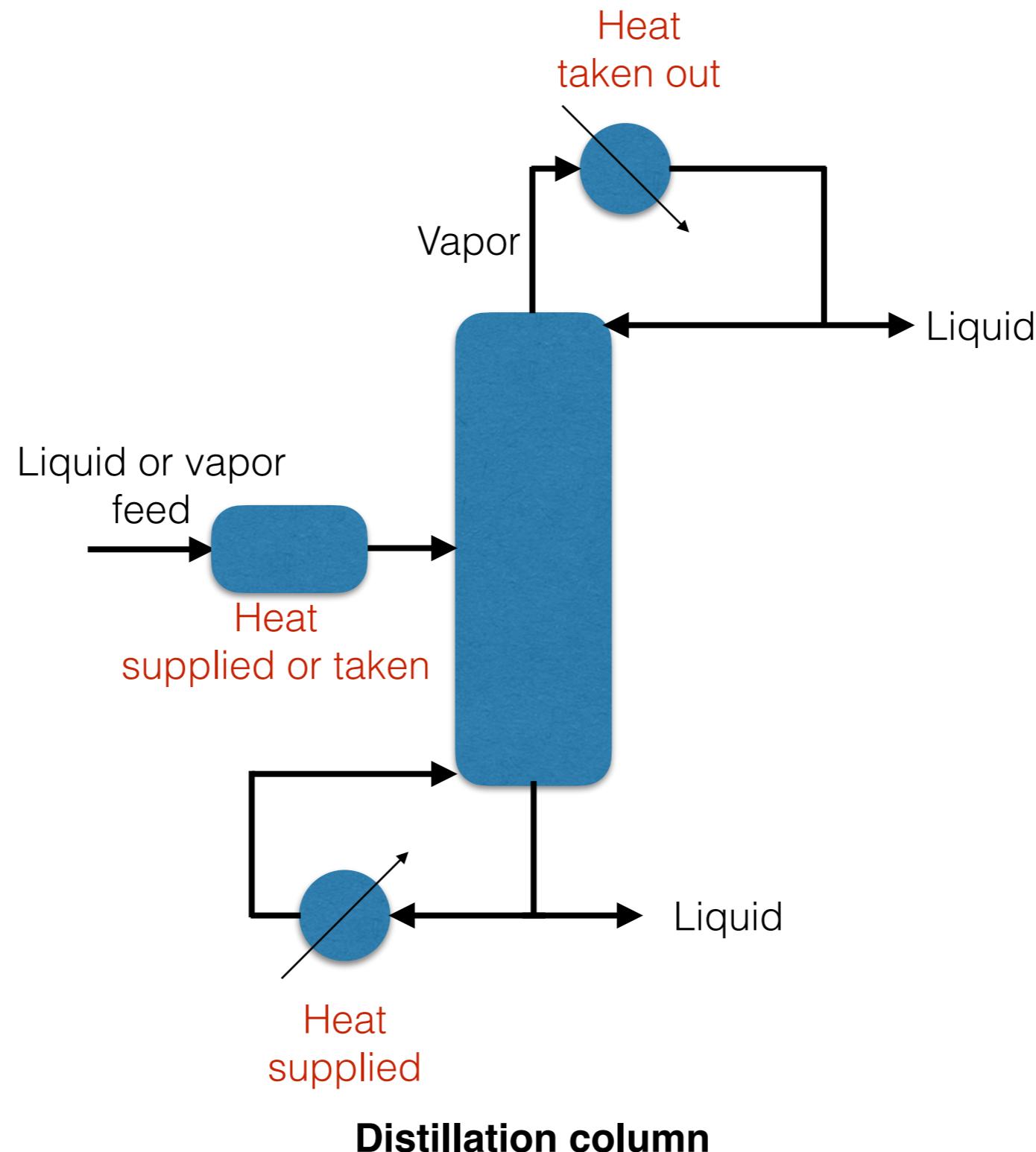
What do we need to know to design these ??



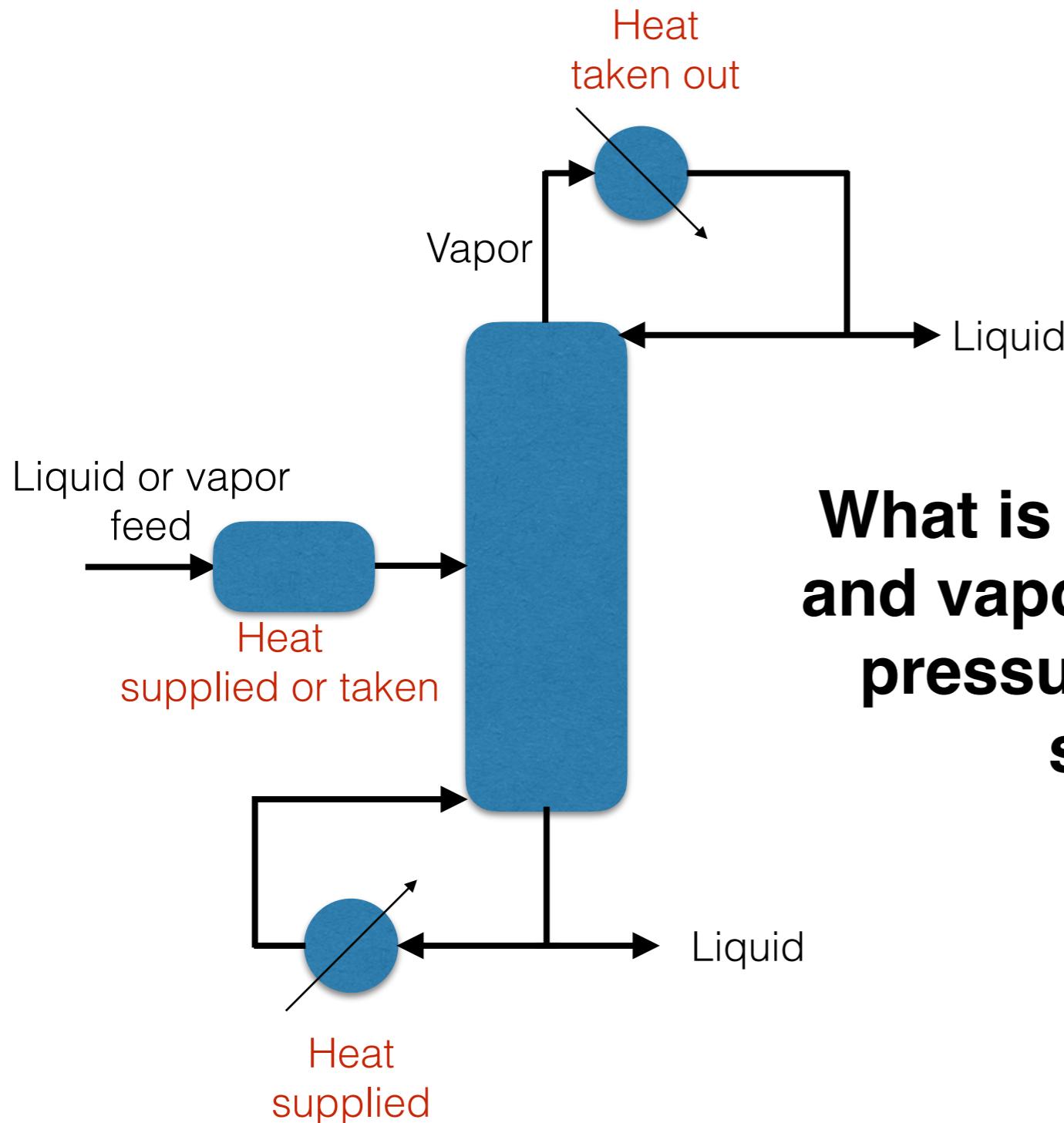
What is the relationship between liquid and vapor concentrations at a given pressure and temperature ???

**Phase equilibria
Mass balance**

Phase creation by energy separating agent (ESA)



What do we need to know to design these ??



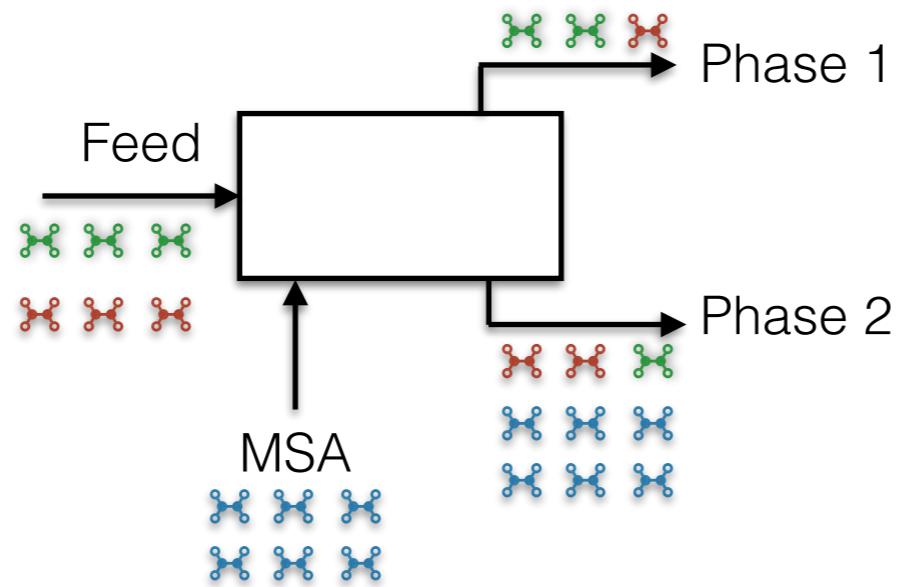
What is the relationship between liquid and vapor concentrations as we change pressure and temperature at several stages of the column ??

**Phase equilibria
Mass balance**

Type of separation process

(2)

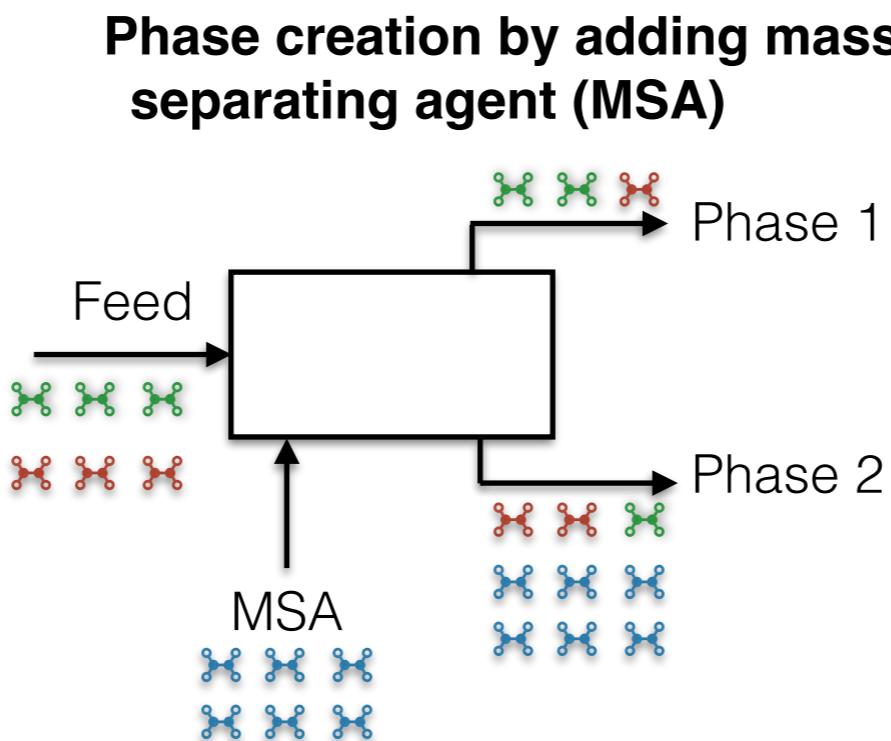
Phase creation by adding mass separating agent (MSA)



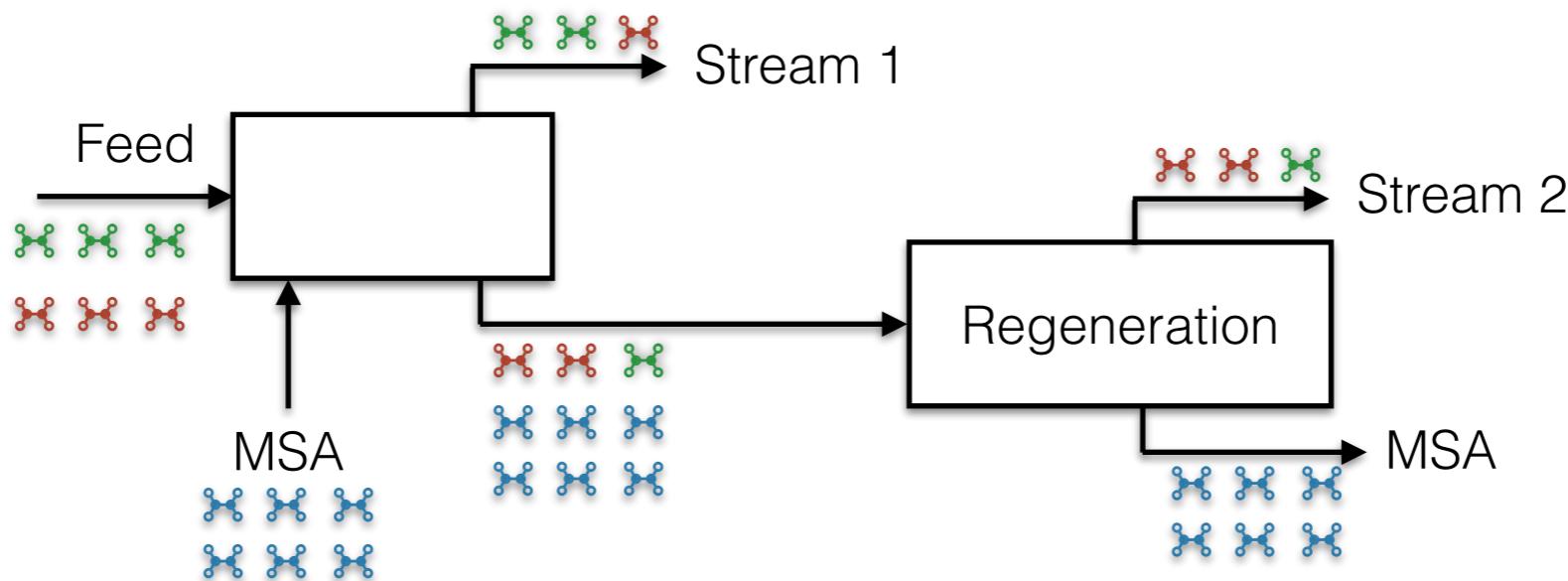
Examples:

1. Absorption
2. Liquid-Liquid Extraction
3. Adsorption

Is the job of separation finished here ?



Regeneration step

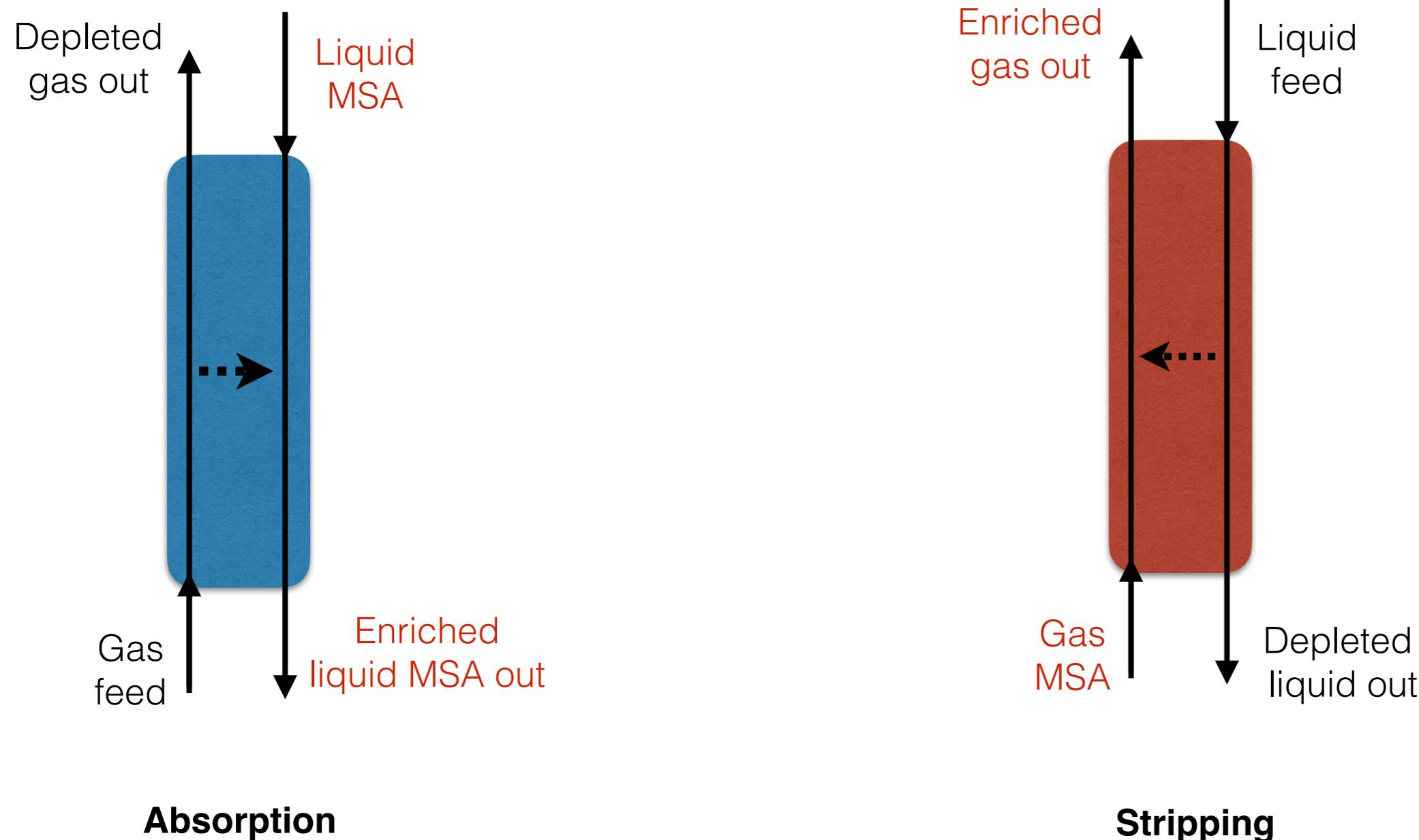


Usually regeneration step is the more expensive step

Potential issues

1. MSA contamination
2. MSA loss
3. MSA degradation

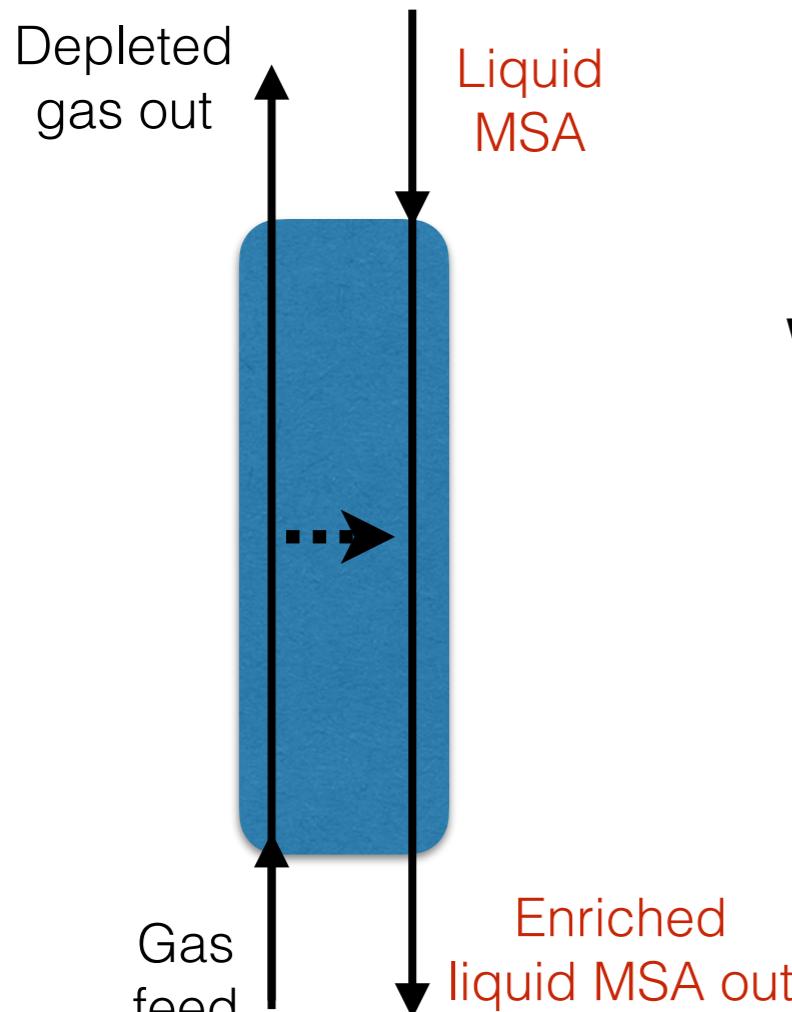
Phase creation by adding MSA



Absorption

Stripping

What do we need to know to design these ??

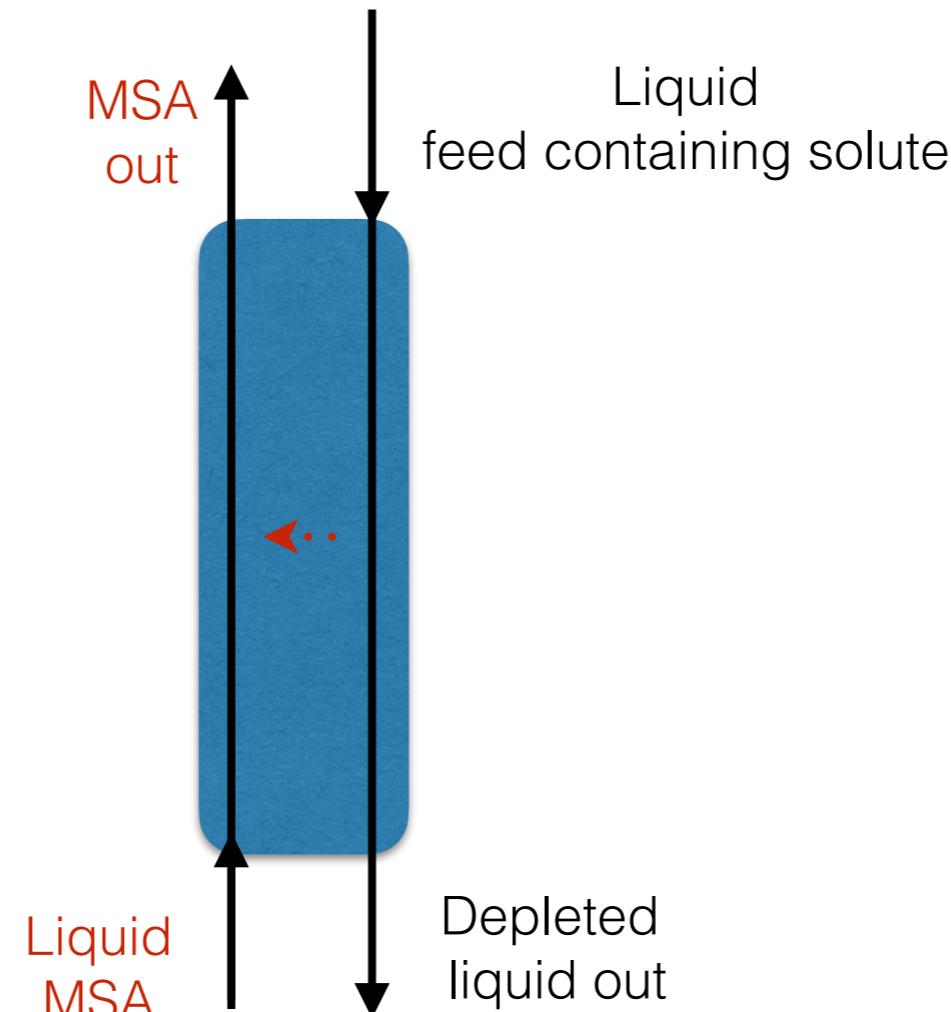


What is the relationship between gas and liquid concentrations at a given pressure and temperature ???

**Solubility data (equilibria)
Mass balance**

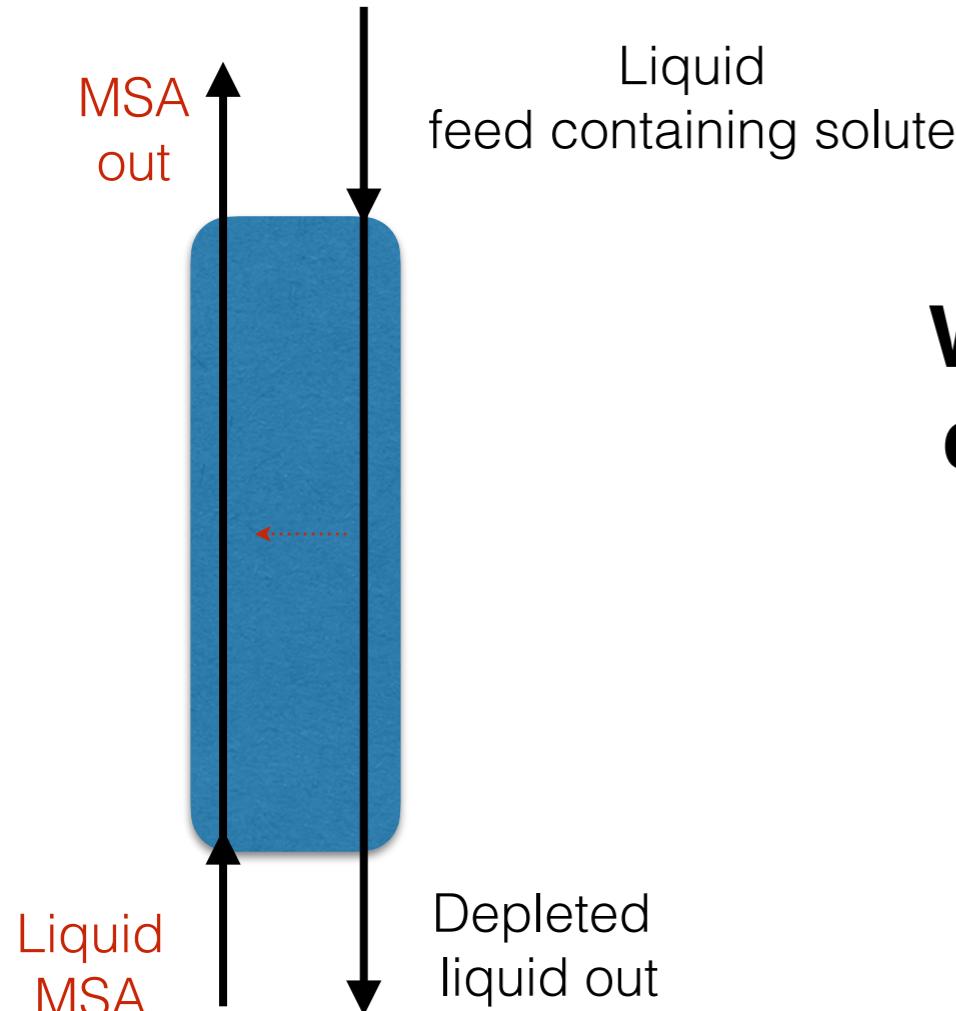
Absorption

Phase creation by adding MSA



Liquid-Liquid Extraction

What do we need to know to design these ??

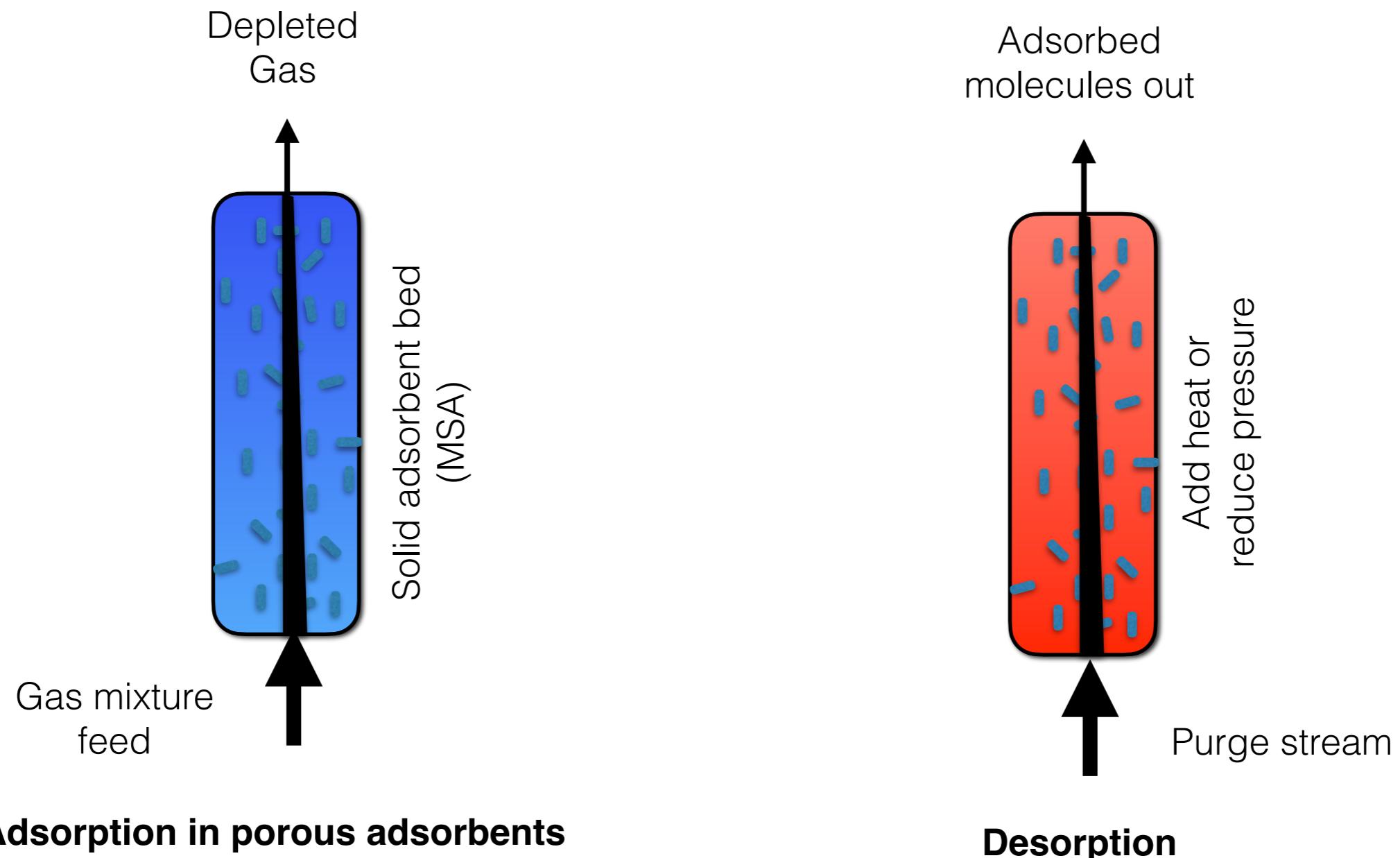


What is the relationship between solute concentration in two liquid phases at a given pressure and temperature ???

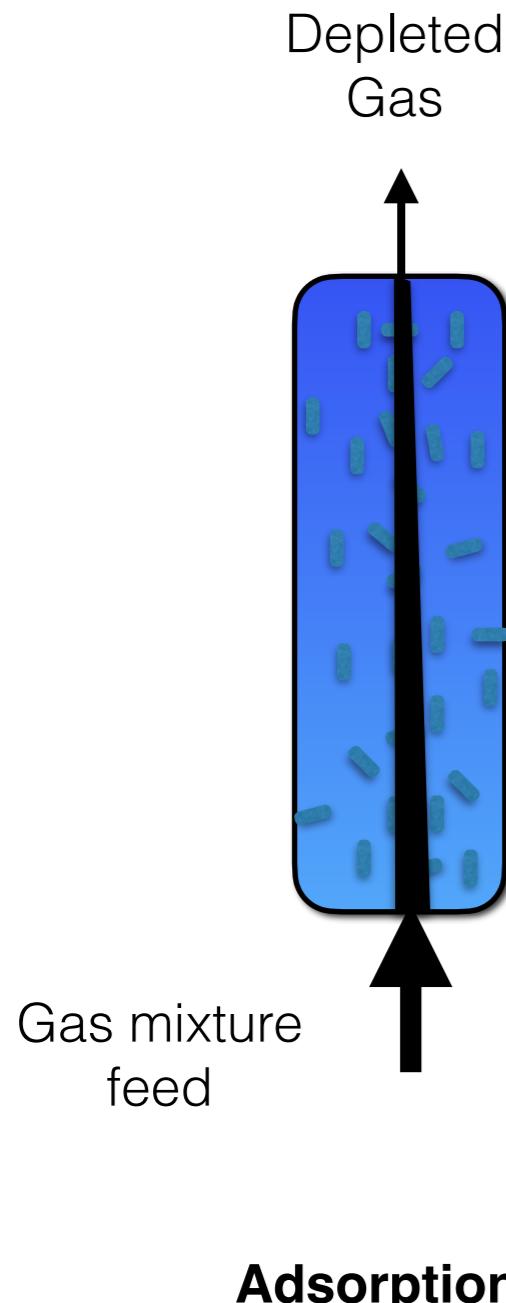
**Solubility data (equilibria)
Mass balance**

Liquid-Liquid Extraction

Phase creation by adding MSA



What do we need to know to design these ??



**What is the relationship between
residence time of two gas components in
the column containing porous adsorbent**

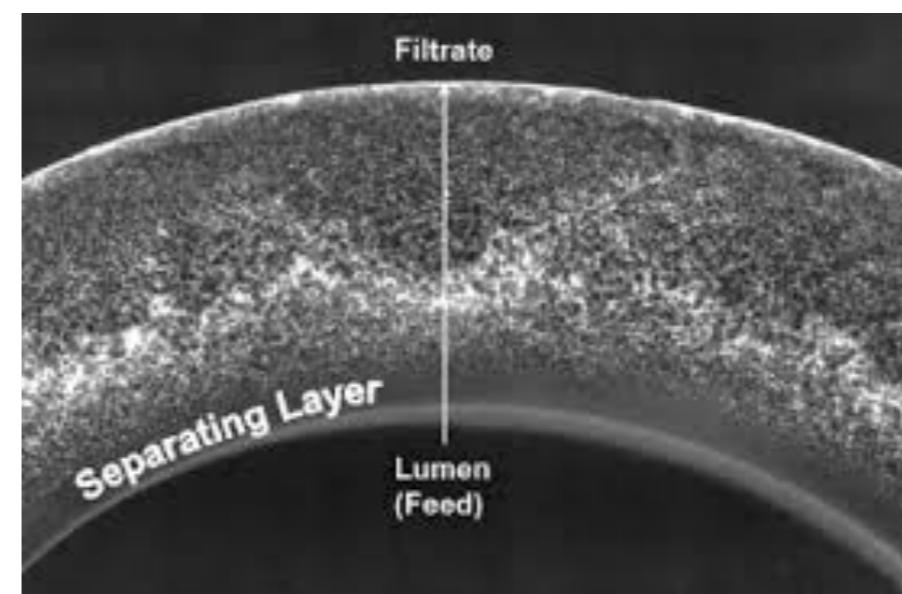
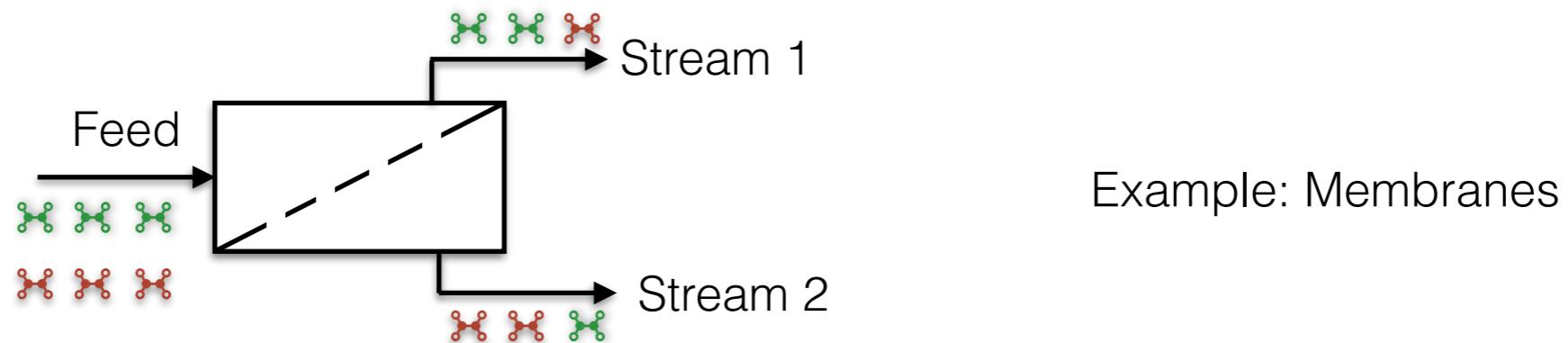
**Binding/adsorption data
Velocity data
Mass balance**

Types of separation using MSA

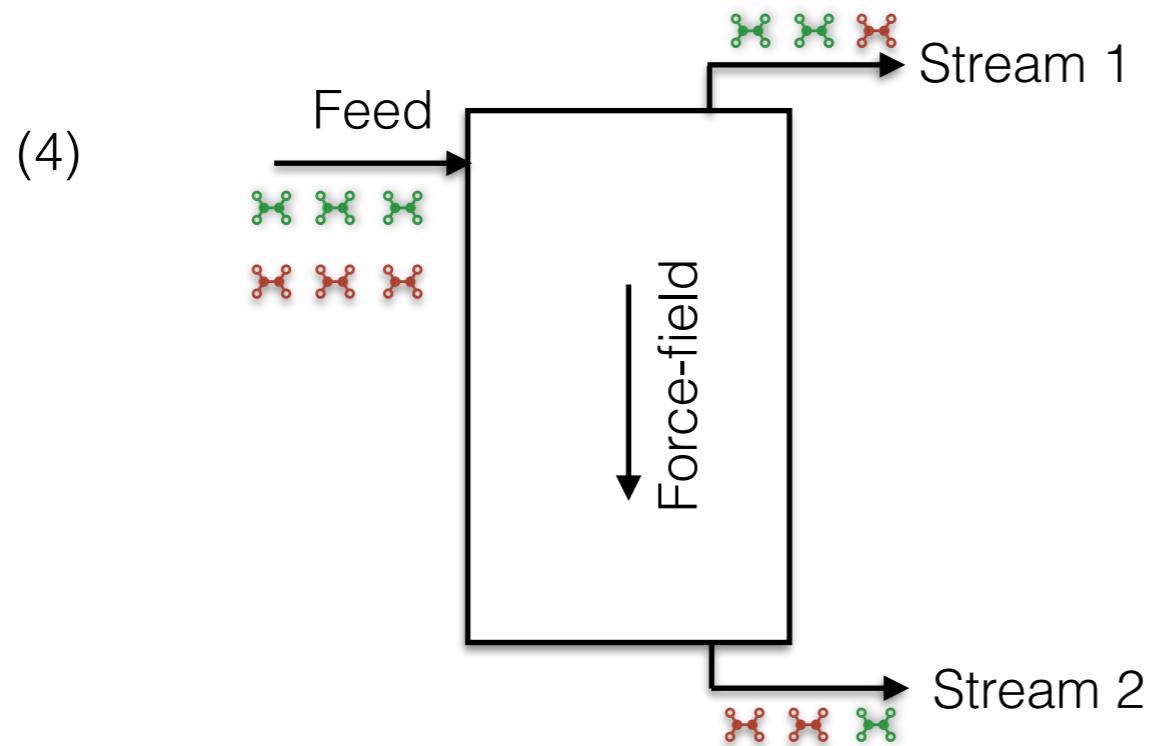
Feed	MSA	Separation	Regeneration Step
Gas	Liquid	Absorption	Stripping
Liquid	Steam	Stripping	Condensation
Solute dissolved in liquid	Liquid solvent	Liquid-Liquid Extraction	Distillation, Stripping, Crystallization
Gas	Porous solid	Adsorption	Desorption

Separation using selective barrier

(3)



Separation using force-field



Example:

- 1) Centrifugation (colloids)
- 2) Electrophoresis (proteins)

Equilibrium vs steady-state

Equilibrium: Thermodynamically balanced properties across interacting system

Thermal Equilibrium

Mechanical Equilibrium

Chemical Equilibrium

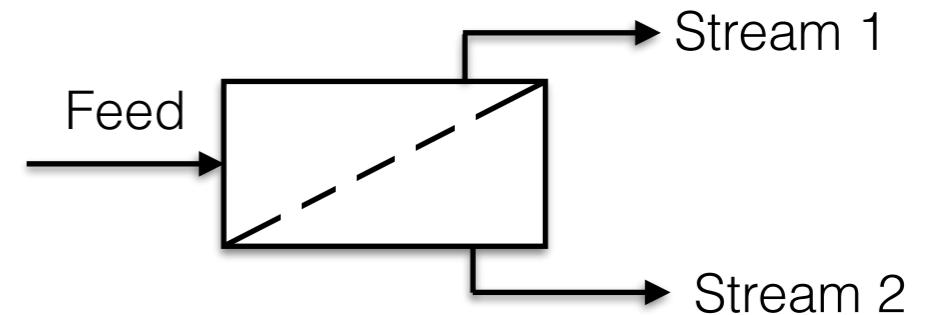
Steady-state: No change in process parameters with respect to time

Distinction of the separation processes

Separation process	Equilibrium-stage	Steady-state
Distillation	Yes	Yes
Absorption	Yes	Yes
Liquid-Liquid Extraction	Yes	Yes
Membranes	No	Yes
Adsorption	No	No

Phase equilibria

What is the relationship between the two streams 1 and 2 in membrane process



- A. They are at equilibrium
- B. They are at steady-state
- C. They are at equilibrium as well as at steady-state
- D. They are neither at equilibrium nor at steady-state

A quick recap of thermodynamics

Specific properties: properties per unit mass

$$\hat{X} = \frac{X}{\text{mass}}$$

Definition of a phase: A region of space where all properties are uniform.

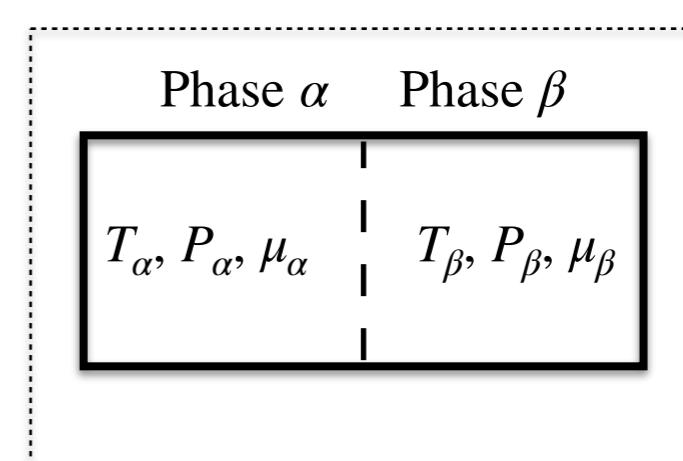
Definition of a steady-state: When properties at a particular point in space do not change with time.

Phase equilibrium: When the temperature, pressure and chemical potential of any component present in one phase is equal to the temperature, pressure and chemical potential of that component in other phase.

$$T_\alpha = T_\beta$$

$$P_\alpha = P_\beta$$

$$\mu_\alpha = \mu_\beta$$



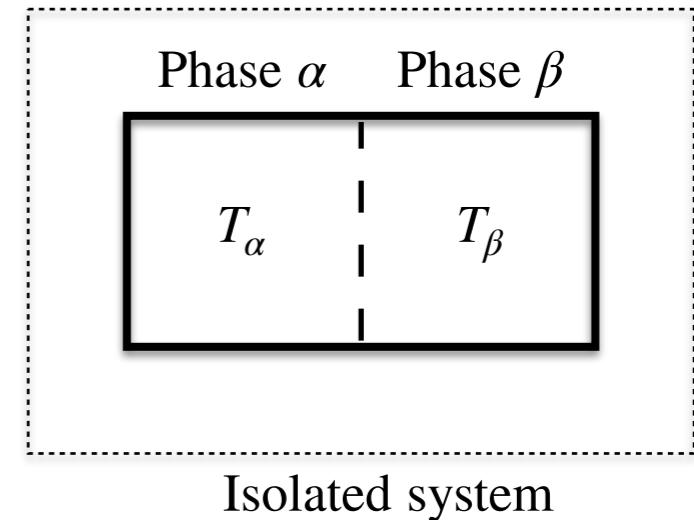
Phase equilibrium: thermal equilibrium

Consider two phases in contact with each other.

The overall system is in isolation.

Temperature of one phase is T_α

Temperature of other phase is T_β



Let's assume that the phases are not in thermal equilibrium $T_\alpha > T_\beta$

As a result a small amount of heat, dq , will flow from phase α to phase β

$$\text{Total entropy change of the system} = dS = -\frac{dq}{T_\alpha} + \frac{dq}{T_\beta} = dq \left(\frac{1}{T_\beta} - \frac{1}{T_\alpha} \right)$$

$$\Rightarrow dS > 0$$

\Rightarrow heat flow will be spontaneous until $T_\alpha = T_\beta$

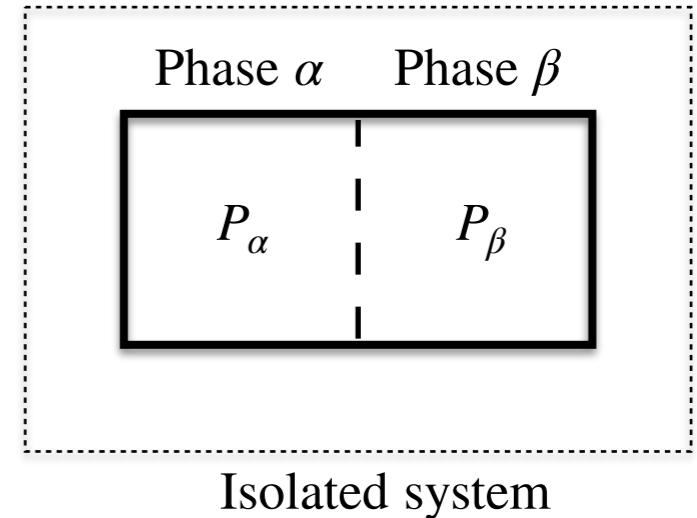
Phase equilibrium: mechanical equilibrium

Consider two phases in contact with each other.

The overall system is in isolation.

Pressure of one phase is P_α

Pressure of the other phase is P_β



Let's assume that the phases are not in mechanical equilibrium $P_\alpha > P_\beta$

As a result, the phase α will expand by small volume dV , and phase β will shrink by the $-dV$

Change in Helmholtz free energy of the entire system $= dA = \sum(-SdT - PdV) = -\sum(PdV) = -P_\alpha dV - P_\beta(-dV)$

$$\Rightarrow dA = dV(P_\beta - P_\alpha) < 0$$

\Rightarrow volume expansion will be spontaneous until $P_\alpha = P_\beta$

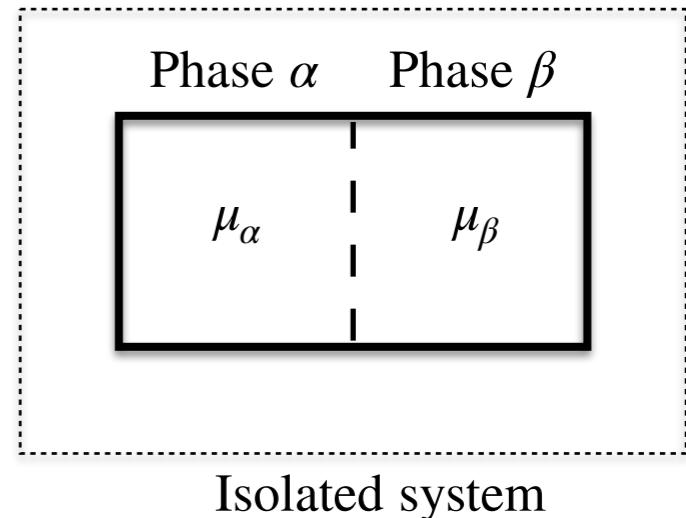
Phase equilibrium: chemical equilibrium

Consider two phases in contact with each other.

The overall system is in isolation.

Chemical potential of one phase is μ_α

Chemical potential of the other phase is μ_β



Let's assume that the phases are not in chemical equilibrium $\mu_\alpha > \mu_\beta$

As a result, a small amount of moles, dN , will transfer from phase α to the phase β

Change in Gibbs free energy of the entire system = $dG = \Sigma(-SdT + VdP + \mu dN) = \Sigma(\mu dN) = \mu_\alpha(-dN) + \mu_\beta(dN)$

$$\Rightarrow dG = -dN(\mu_\alpha - \mu_\beta) < 0$$

\Rightarrow mole transfer will be spontaneous until $\mu_\alpha = \mu_\beta$

Degree of Freedom \mathcal{F}

$$\mathcal{F} = \text{number of variables} - \text{number of equations}$$

Typically, number of variables are more than number of equations.

The knowledge of the degree of freedom for a given system allows us to choose number of independent variables.

$\mathcal{F} = 3$, then one can assign 3 independent variables : P, T, mole fraction

$\mathcal{F} = 2$, then one can assign 2 independent variables : T, mole fraction

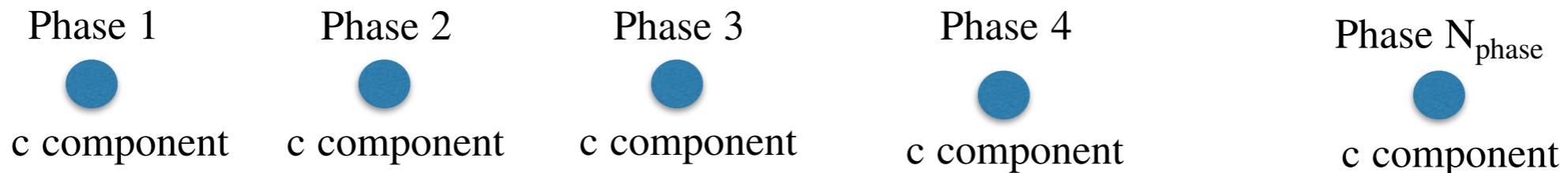
$\mathcal{F} = 1$, then one can assign 1 independent variables : mole fraction

It would be nice to have some guideline which can tell us about \mathcal{F}

For phase equilibria, Gibbs phase rule : $\mathcal{F} = 2 - N_{\text{phase}} + N_{\text{component}}$

Derivation for Gibbs phase rule

Consider a system with c component where several phases (N_{phase}) are in equilibrium with each other.



Total number of variables: P, T, mole fraction of all c component in each phase $= 2 + cN_{phase}$

Total number of equations:

Mole fraction in each phase add up to 1

$$\Rightarrow \sum_{i=1}^c x_i^{phase\ k} = 1, \text{ for } k = 1, 2, 3, \dots, N_{phase}$$

Number of such equation = N_{phase}

Equilibrium relationships

$$x_i^{phase\ 1} = k_{i,12} x_i^{phase\ 2}$$

Number of such equation for each component = $N_{phase} - 1$

Total number of such equations = $c(N_{phase} - 1)$

$$\text{Total equations} = N_{phase} + c(N_{phase} - 1)$$

$$\text{Total number of independent variables} = 2 + cN_{phase} - (N_{phase} + c(N_{phase} - 1)) = 2 - N_{phase} + c$$

Vapor-liquid equilibrium (2 component)

$$Py_1 = \gamma_1 x_1 P_{1,sat}$$

where, $P_{1,sat} = f(T)$

$$\gamma_1 = g(T, x_1)$$

$$k_1 = \frac{\gamma_1 P_{1,sat}}{P}$$

$$\Rightarrow y_1 = k_1 x_1$$

$$\mathbf{y_1} = \mathbf{f(T, P, \gamma_1, x_1)}$$

For ideal solution, $\gamma_1 = 1$

$$Py_1 = x_1 P_{1,sat}$$

Roult's law

$$k_1 = \frac{P_{1,sat}}{P}$$

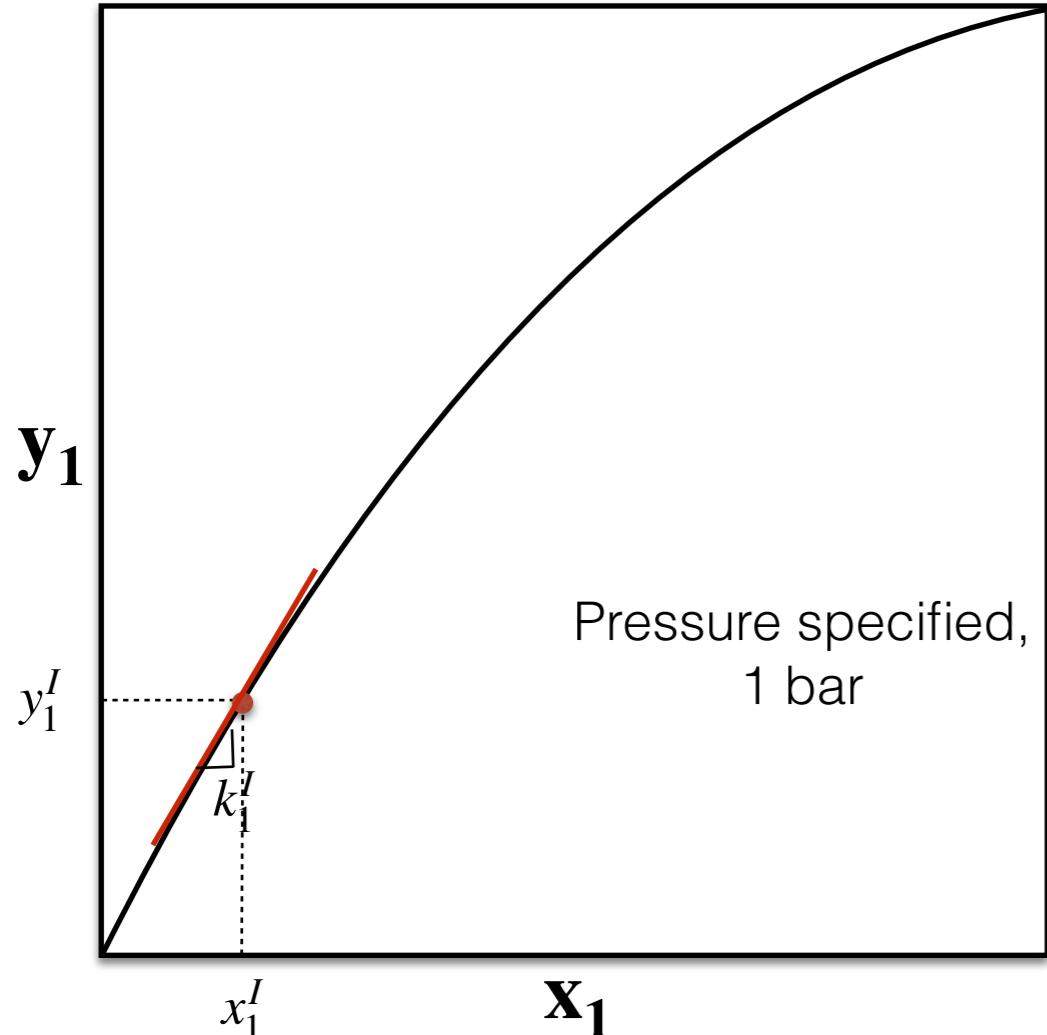
$$y_1 = \frac{P_{1,sat}}{P} x_1$$

\mathcal{F} for 2 component, 2 phase = 2

Any of these set of variables can be specified : (T, x_1) , (P, x_1) , (T, P) , (x_1, y_1)

Sometime, instead of temperature/pressure, specific enthalpy is specified

Graphical methods: y-x diagram

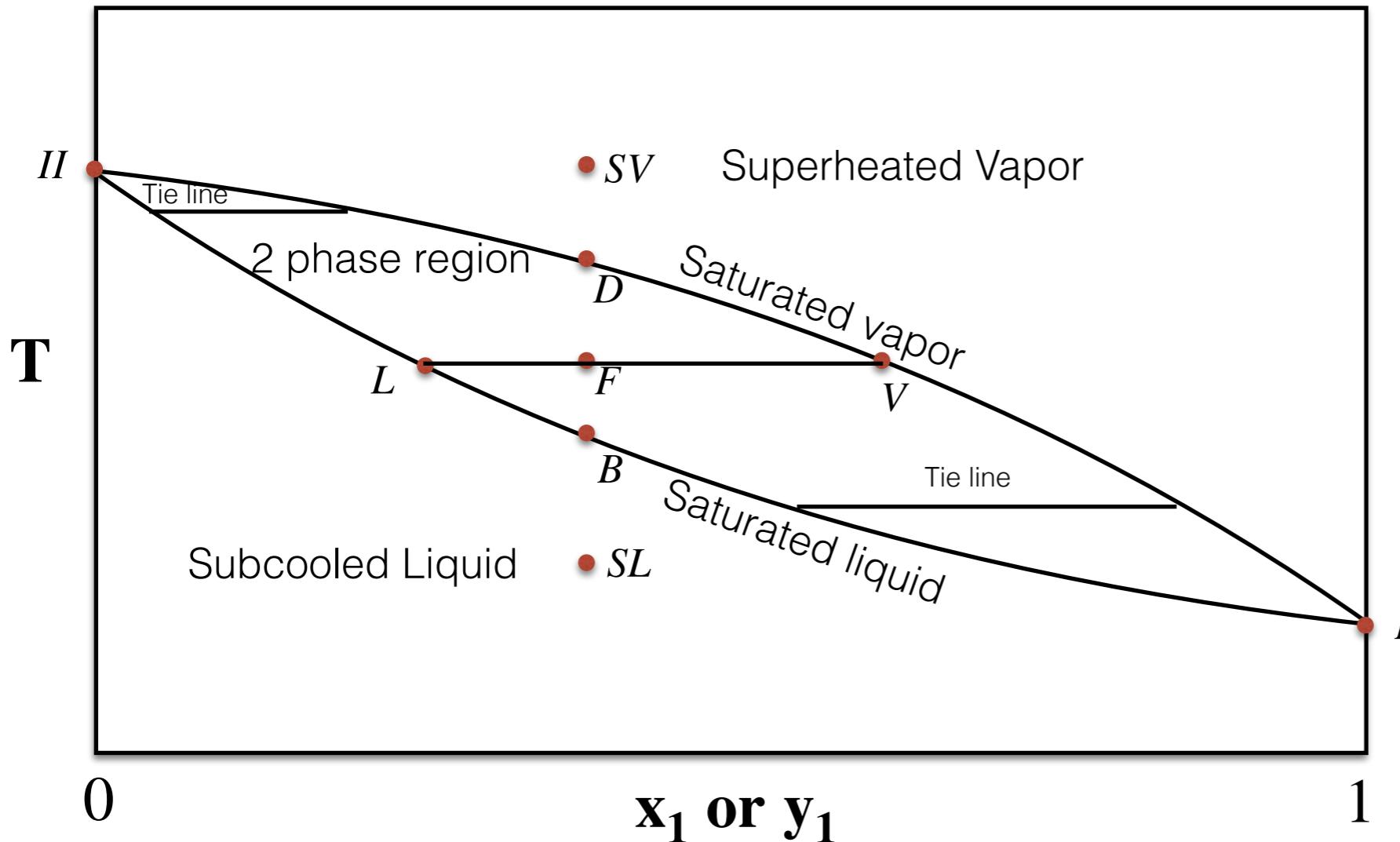


$$Py_1 = \gamma_1 x_1 P_{1,sat}$$

$$k_1^I = \frac{\gamma_1 P_{1,sat}}{P}$$

$$y_1^I = k_1^I x_1^I$$

Graphical methods: T-x-y diagram for liquid-vapor phase



T_D = Dew point : temperature at which liquid droplets first appear in saturated vapor

T_B = Bubble point : temperature at which vapor bubbles first appear in saturated liquid

Graphical methods: T-x-y diagram for liquid-vapor phase

What is special about points I and II ?

